

Modelling of Multi-Parameter-Level Simulation Data to Create an Enhanced Cordier Diagram for Radial Turbocompressors



iSimT-24 Symposium on Innovative Simulations in Turbomachinery

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1. Introduction
2. Computational Model
3. Nested Design of Experiments
4. Surrogate Modeling
5. Applications

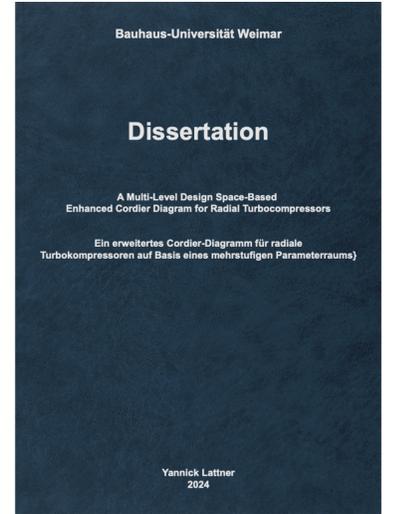


INTRODUCTION

Parameterization, simulation and data-modeling
as an integral part of the PhD-thesis:

*A Multi-Level Design Space-Based
Enhanced Cordier Diagram for Radial
Turbocompressors*

(Currently being reviewed at Bauhaus-Universität Weimar)

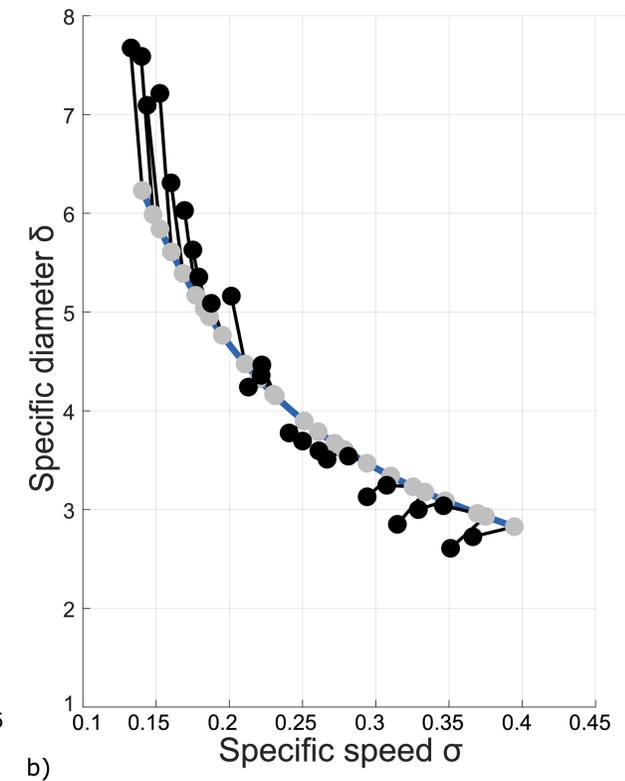
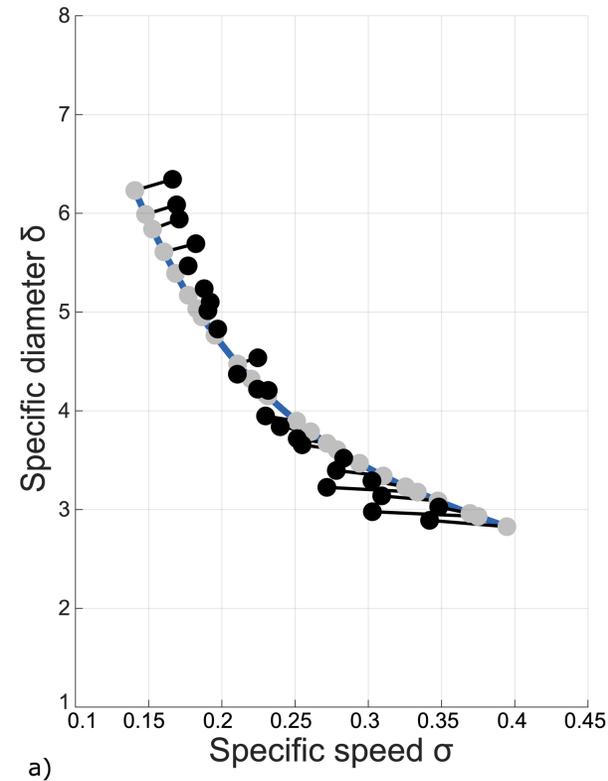


INTRODUCTION

Concept of the enhanced Cordier diagram

The Cordier diagram

- Shall provide combinations of specific speed σ and specific diameter δ using the Cordier line
- Iterations of rotational velocity or diameter to obtain feasible designs, change the location in the Cordier diagram
- Cordier line is not a functional, precise approach for modern radial turbocompressor designs

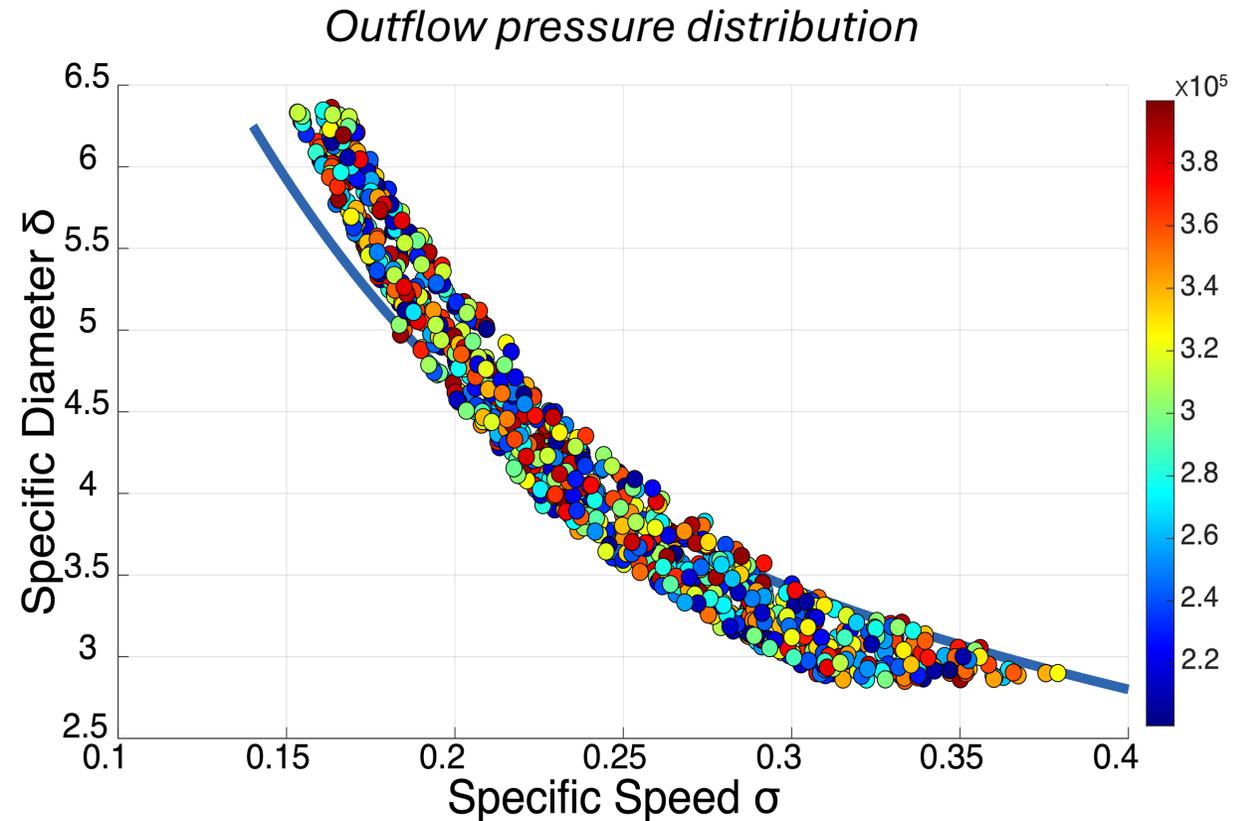


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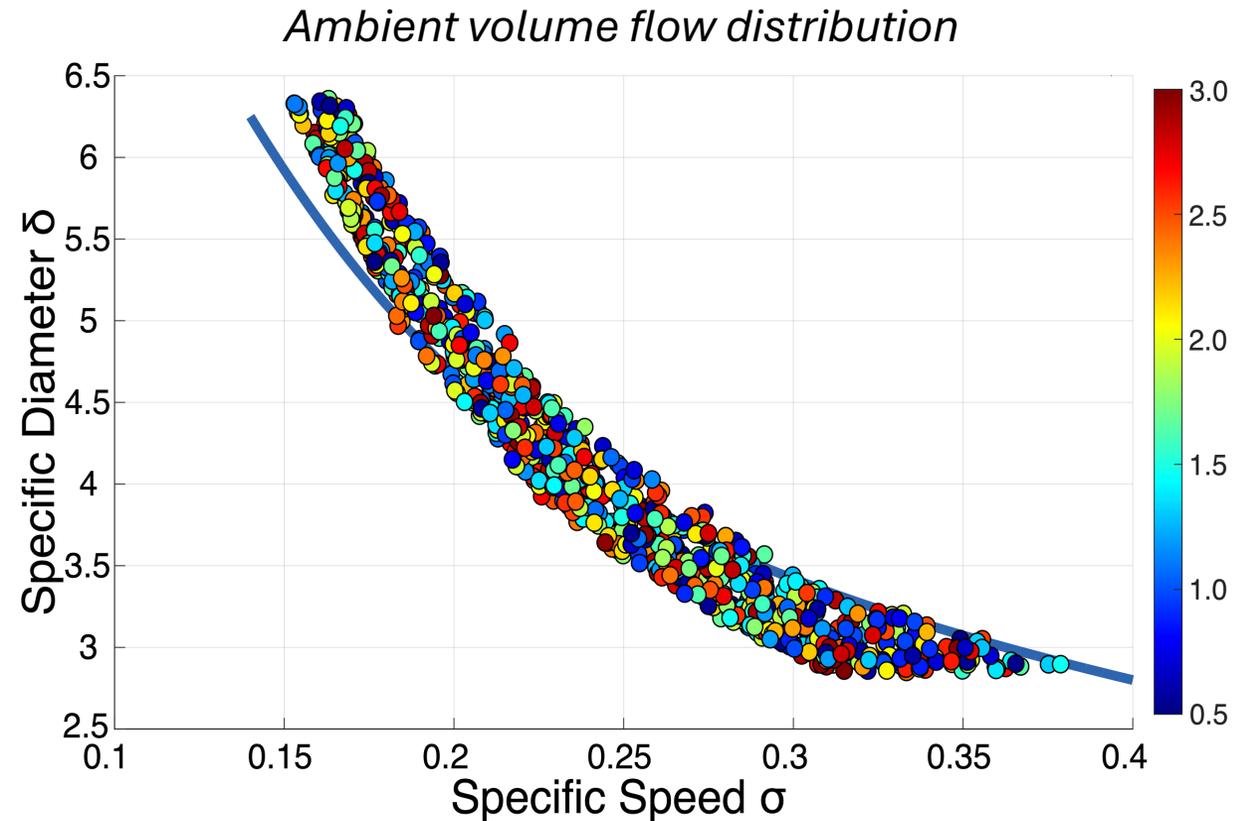


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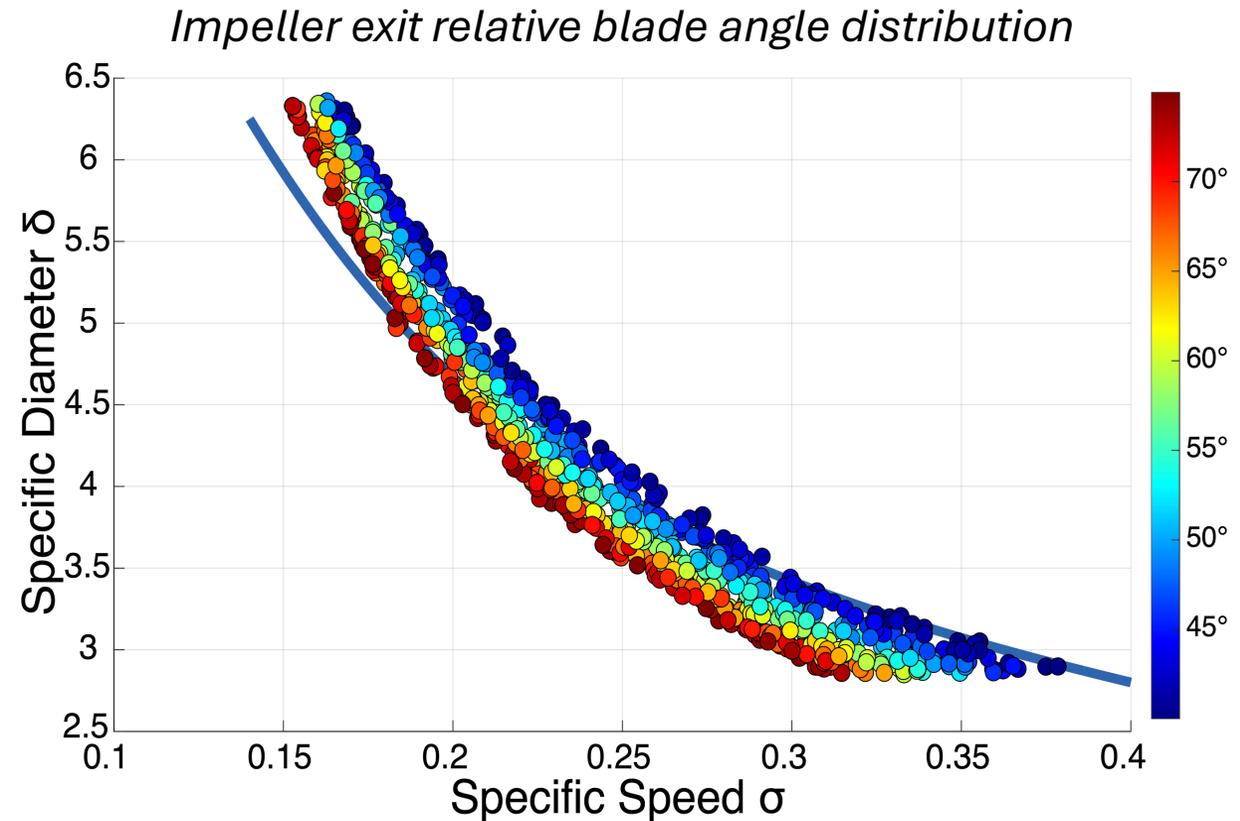


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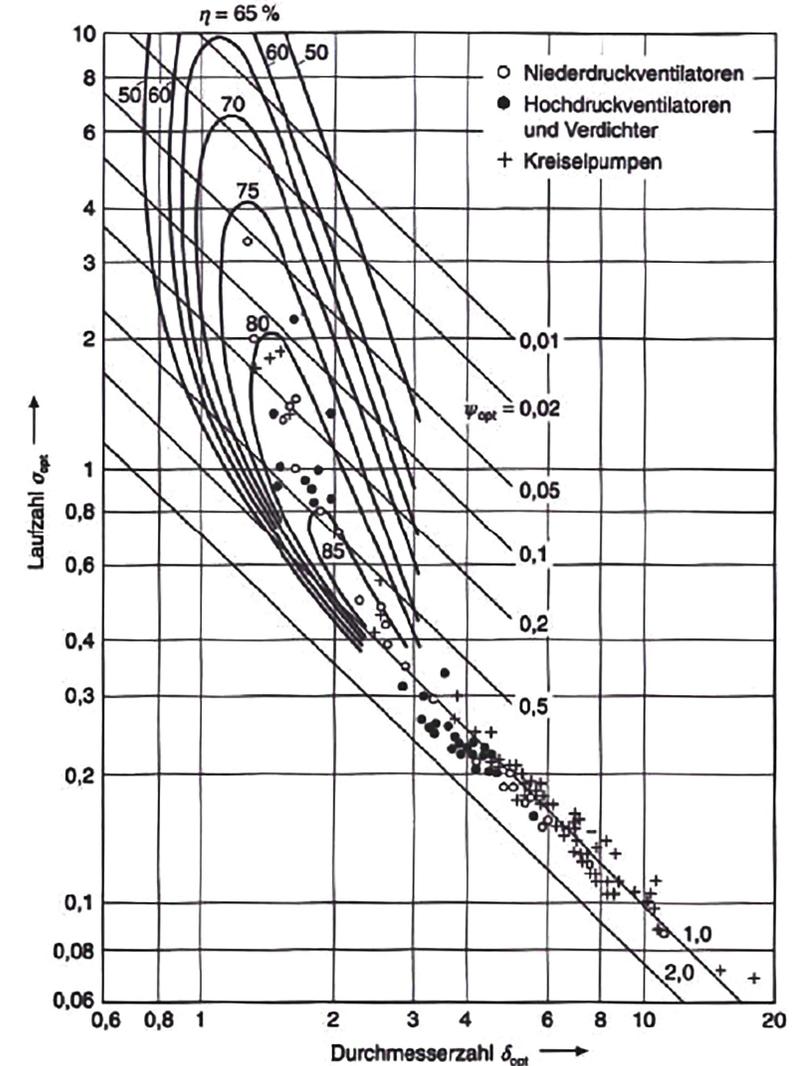


INTRODUCTION

Concept of the enhanced Cordier diagram

The Cordier diagram

- Fails to provide precise combinations of rotational velocity and impeller diameter for modern machines
- Does not provide any indication regarding a future compressor's efficiency
- Neglects significant parameter influences



INTRODUCTION

Concept of the enhanced Cordier diagram

A digital, enhanced Cordier Diagram

- Re-enable the indented use
- Provide additional data to weight possible designs
- Operate as a digital tool with application-based outputs
- **Based on simulation data of modern radial turbocompressors**
- Inputs must be available at the start of the design process

INTRODUCTION

Requirements to the computational model

- Complex parameter space
 - Differentiation of influences introduced by geometry design space and machine design space
 - Machine design process
 - Parameterized CAD Geometry
 - CFD-based speed line computation
 - Structural simulation (FEA)
- Automated workflow
- Compatible parameter spaces

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COMPUTATIONAL MODEL

Machine Design Model

- Inputs:

- Ambient conditions
- Outflow pressure
- Ambient volume flow
- Axial impeller extent ratio
- Impeller exit relative blade angle
- Circumferential blade extent
- Number of blades
- ...

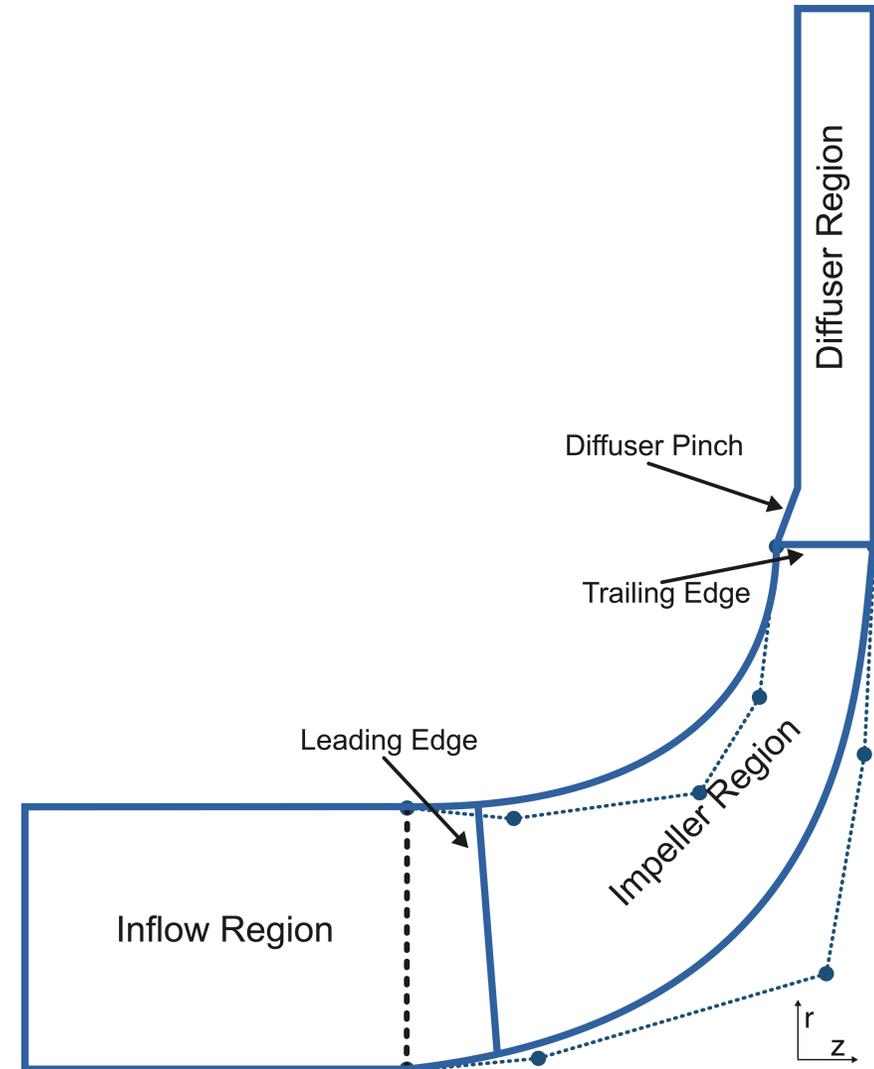
- Outputs:

- All principal dimensions
 - Diameters
 - Blade angles
 - Thermodynamic properties
 - Chord Reynolds number
 - ...

COMPUTATIONAL MODEL

Geometry Design

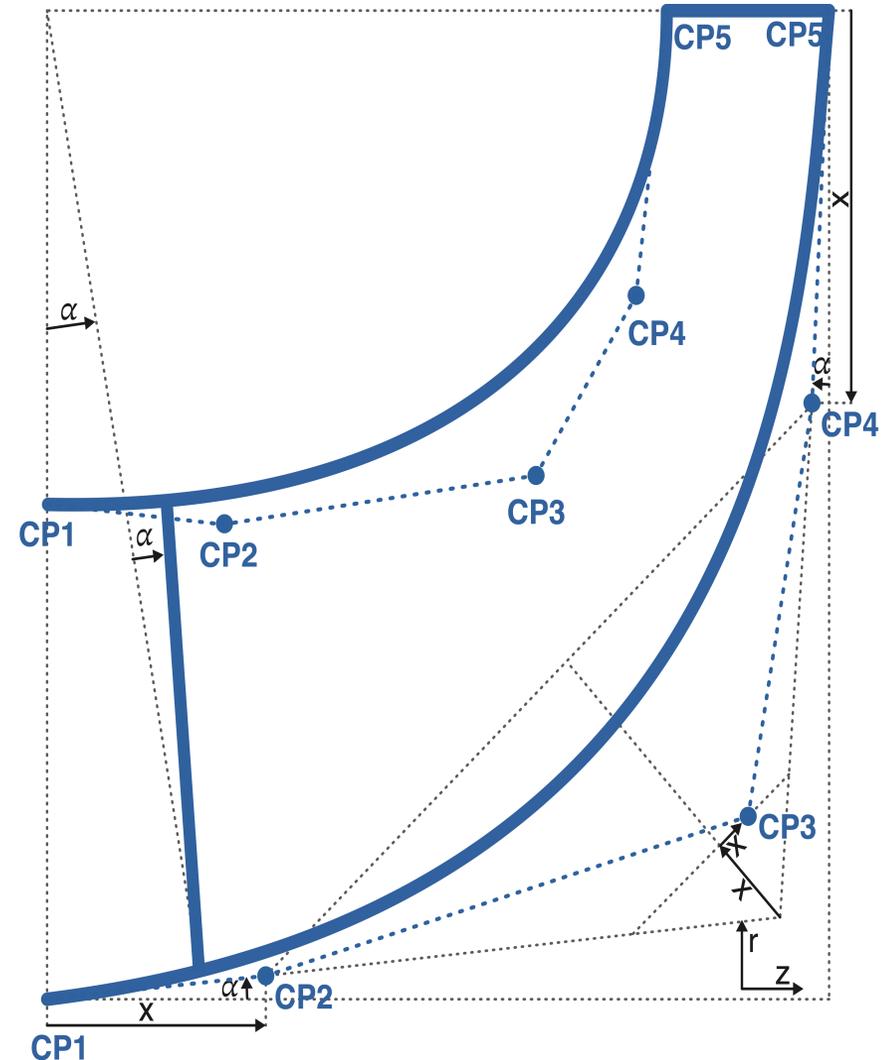
- Based on non-dimensional parameters (Angles / ratio to D_2)
- Including parameterized impeller disc
- Reduced parameter set controls multiple design parameters by global parameters



COMPUTATIONAL MODEL

Geometry Design

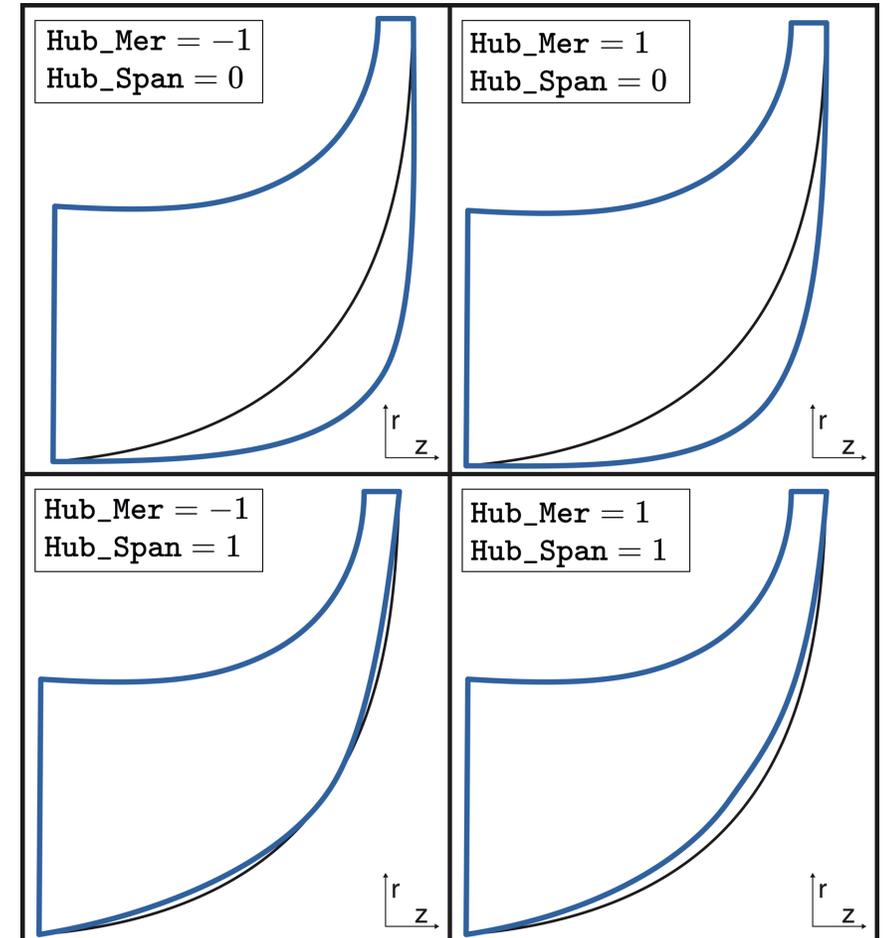
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COMPUTATIONAL MODEL

Geometry Design

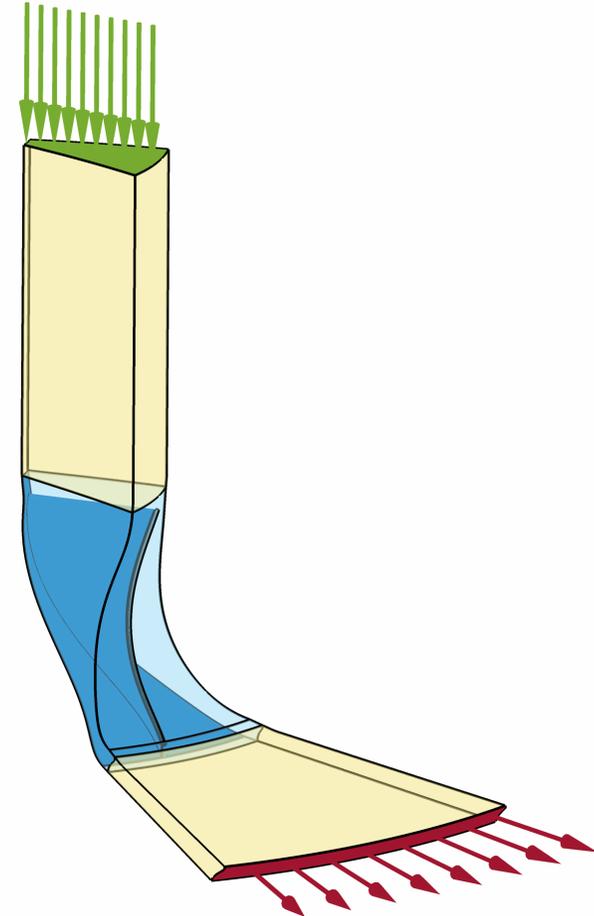
- Reduced parameter set controls multiple design parameters by global parameters
- Allows for significant reduction of sample size with neglectable reduction of result parameter range



COMPUTATIONAL MODEL

CFD Model

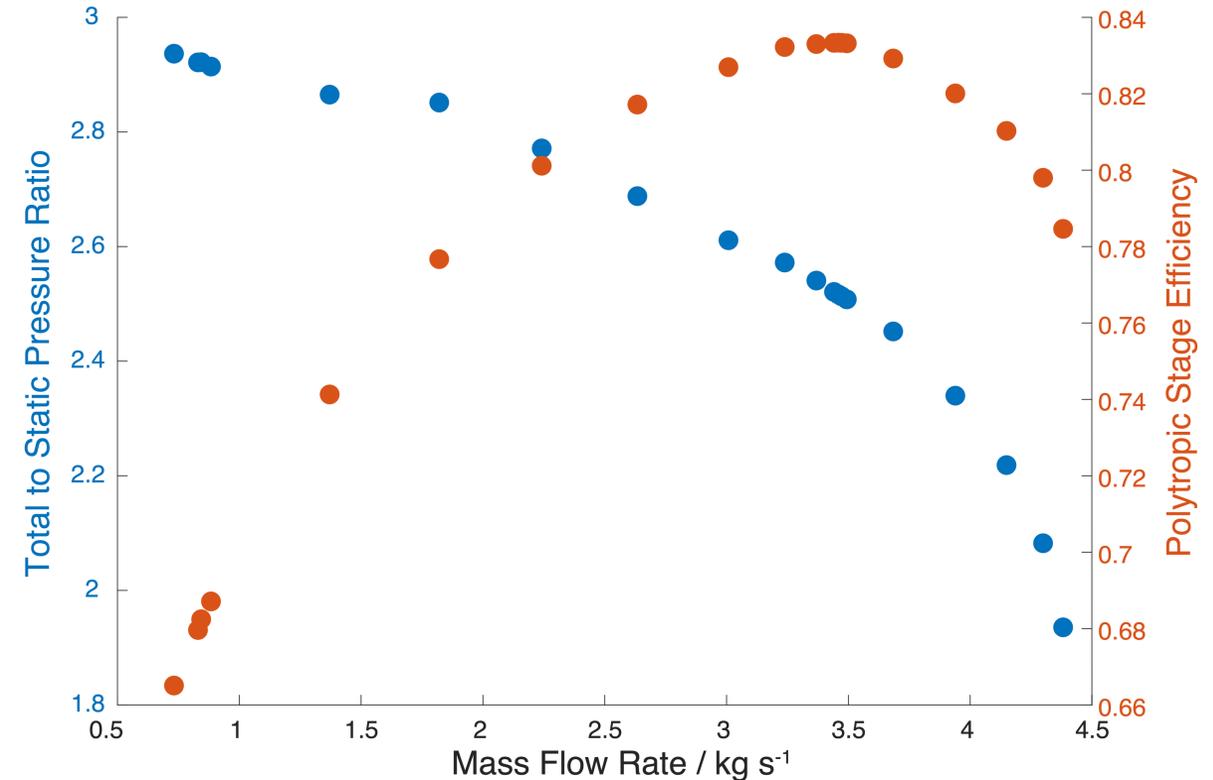
- CFX Turbomachinery Setup
- Exit-corrected mass flow rate
- Convergence evaluation using CoV
- Averaging approach for unsteady results



COMPUTATIONAL MODEL

Speed Line Computation

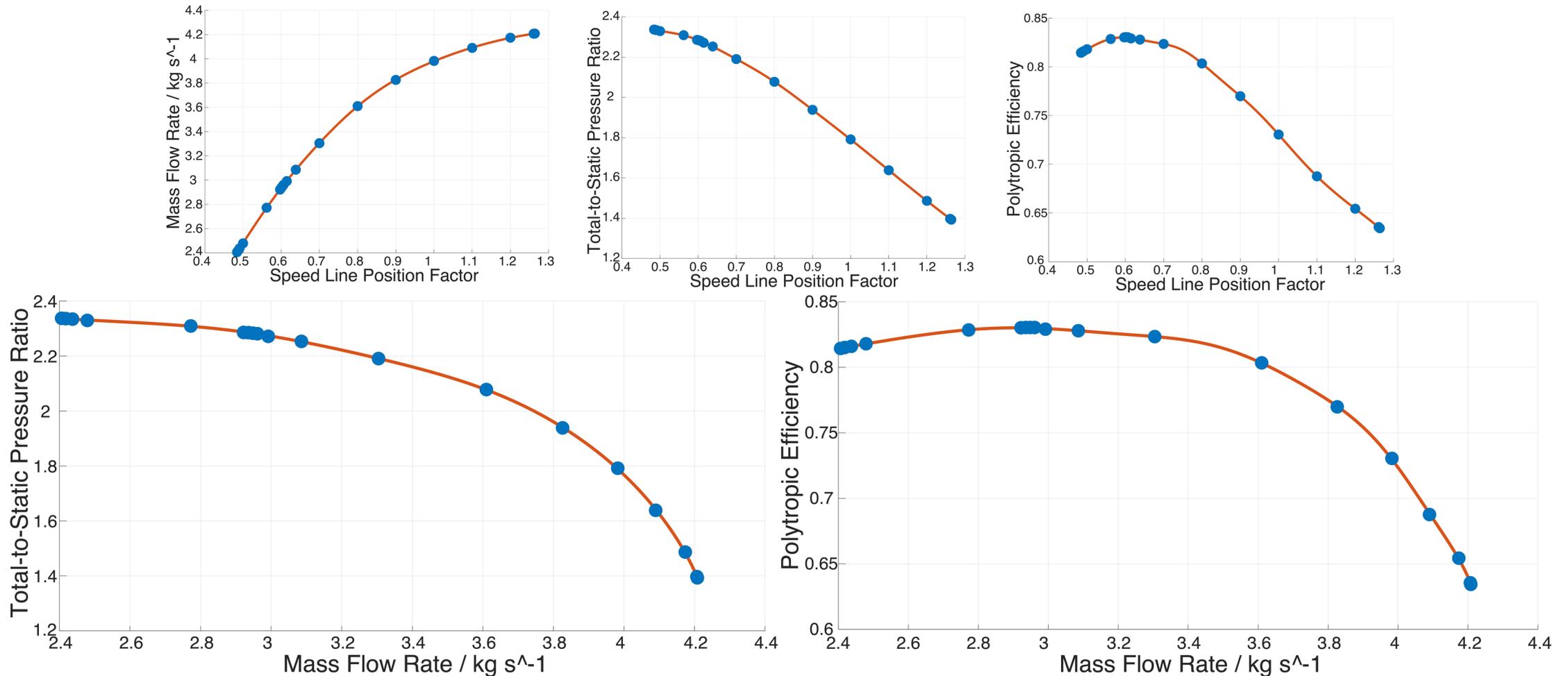
- Fully automated speed line computation tool ¹⁾
- Choke point defined at quasi-constant mass flow rate
- Surge at maximum of static outflow pressure
- Direct Peak-Efficiency point identification



¹⁾“Physics-Based Surge Point Identification for Unsupervised CFD-Computation of Centrifugal Compressor Speed Lines” in Energy Conversion and Management: X, Yannick Lattner, Marius Geller and Michael Kutz, DOI: [10.1016/j.ecmx.2022.100337](https://doi.org/10.1016/j.ecmx.2022.100337)

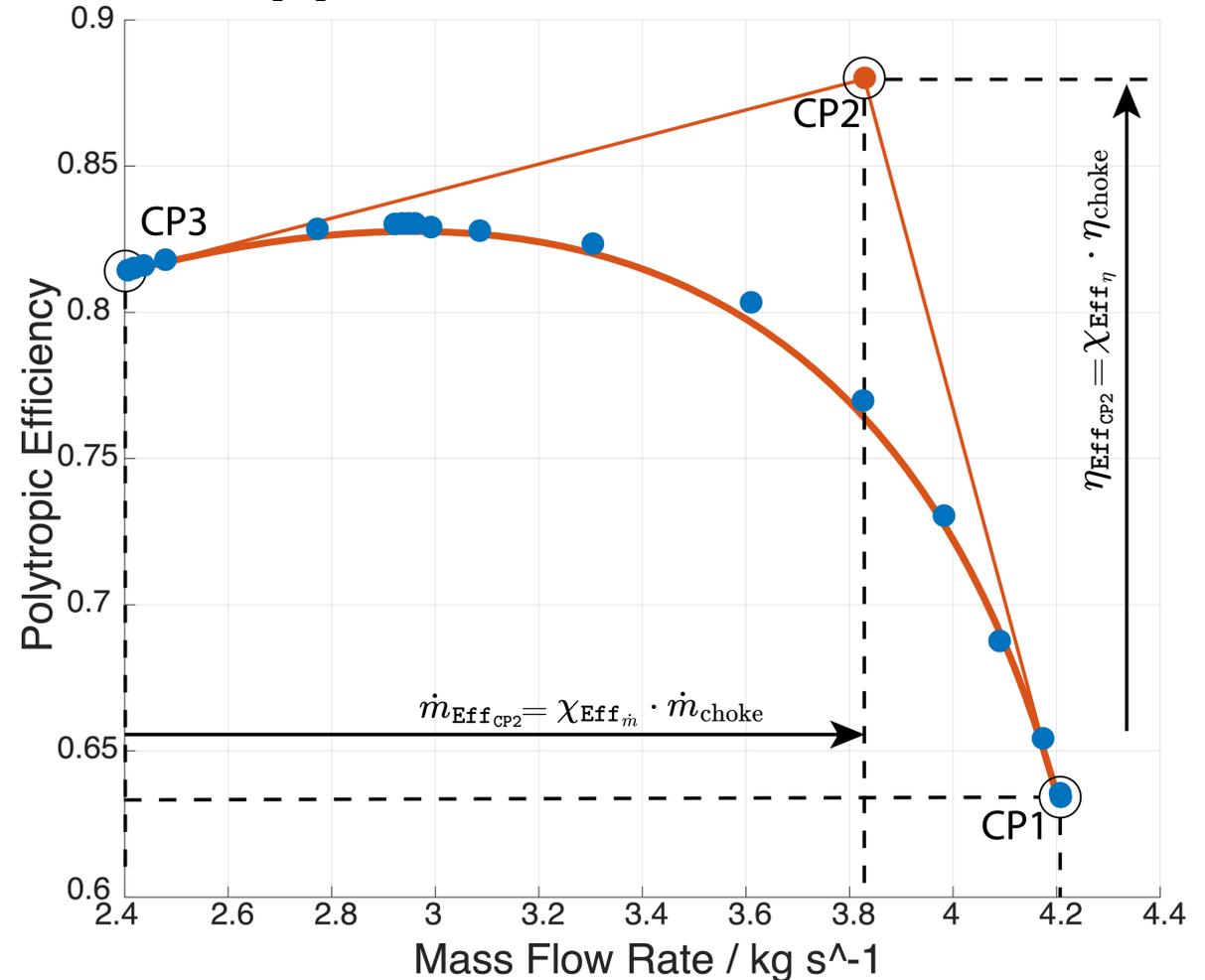
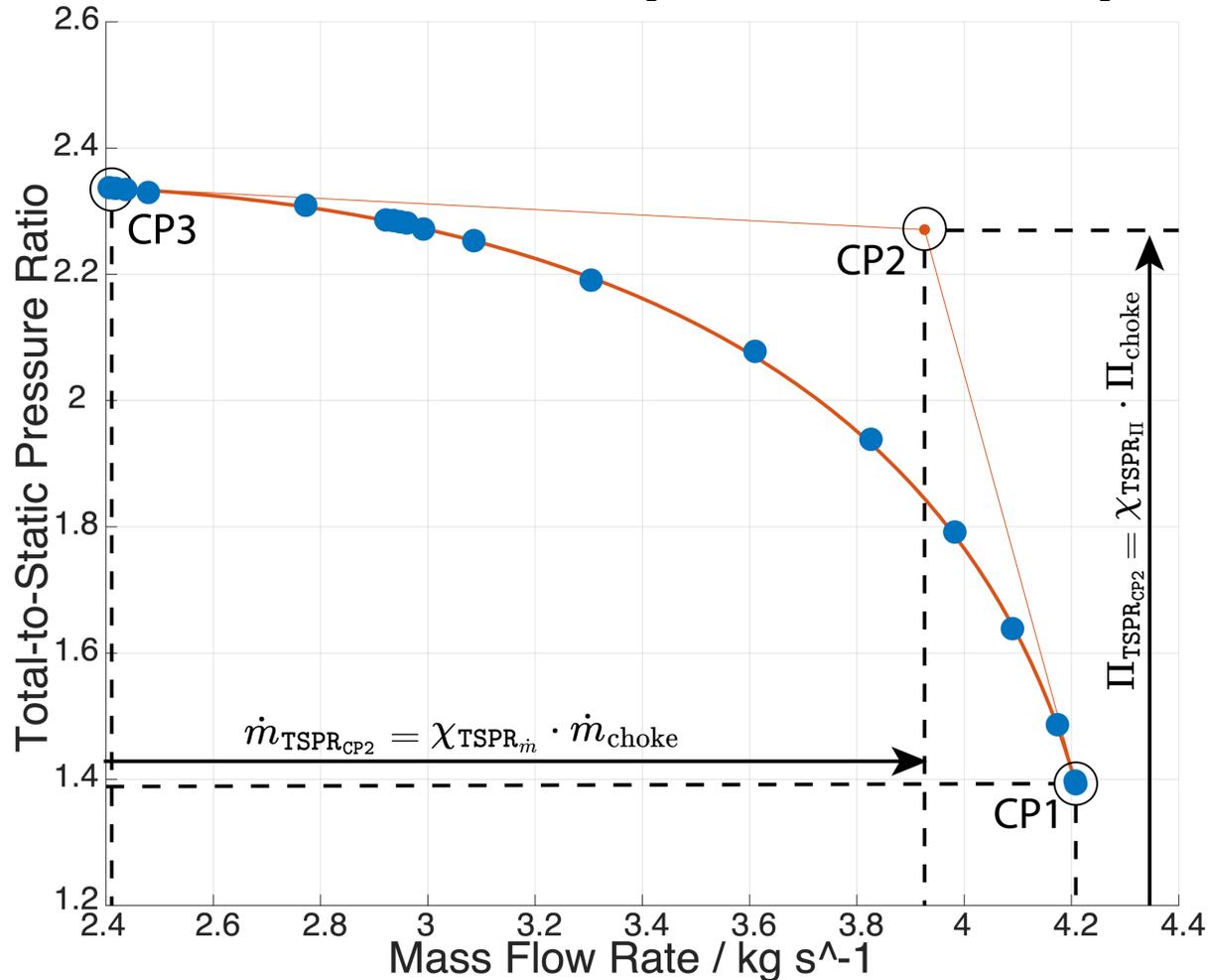
COMPUTATIONAL MODEL

Neural network-based speed Line interpolation



COMPUTATIONAL MODEL

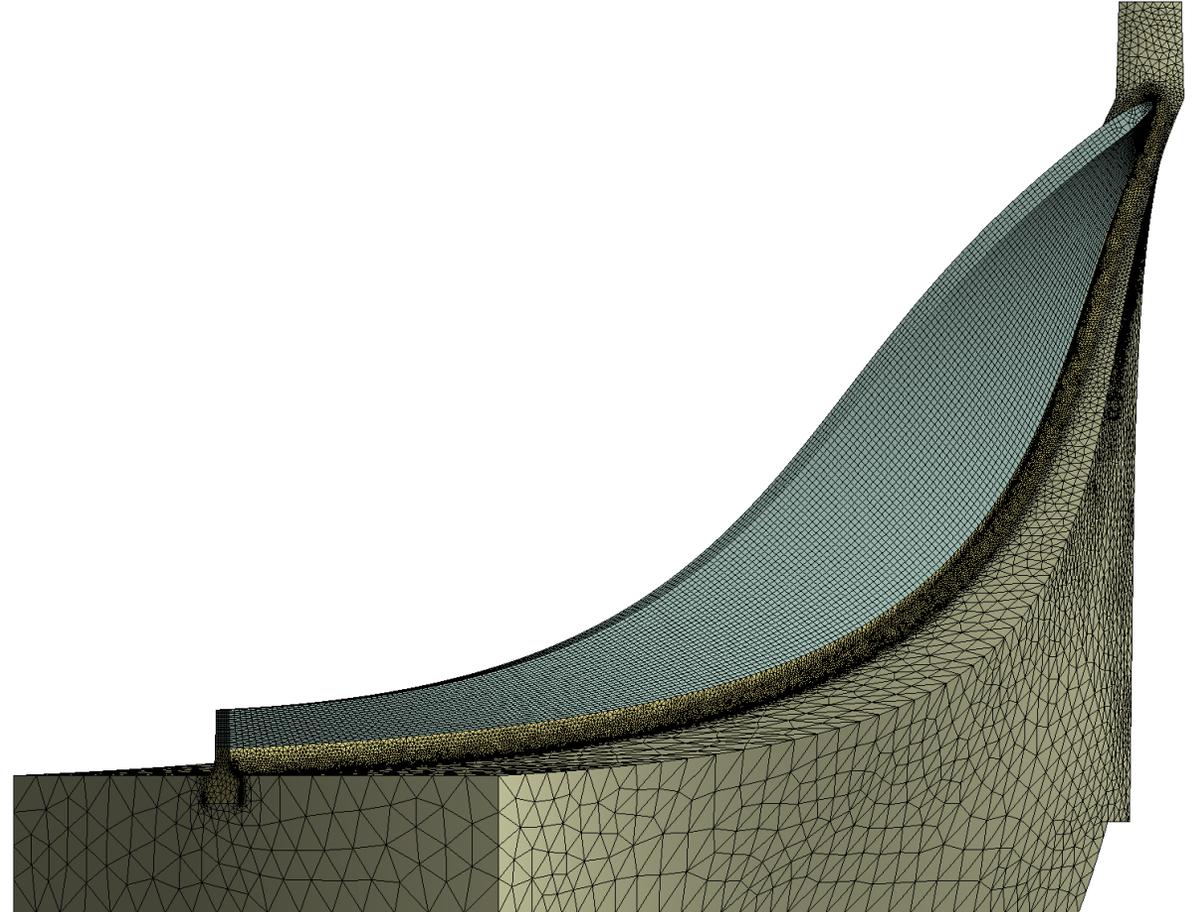
Low order, Bézier spline-based speed Line approximation model



COMPUTATIONAL MODEL

FEA Model

- Load due to rotational velocity
- No thermal or dynamic effects
- Evaluation of:
 - Maximum deformation and von-Mises stress
 - Leading and trailing edge deformations
 - Elastic strain energy (density) for multiple partitions



COMPUTATIONAL MODEL

Hybrid Surrogate modeling

- Flexible and universal approach to surrogate modeling using multiple component surrogate models (CSMs)
- Each component surrogate model is individually trained
- Hybrid surrogate model is composed by all by optimizing individual weights
- In this approach, combination of:
 - Polynomial regression
 - Neural networks
 - Kriging

COMPUTATIONAL MODEL

Hybrid Surrogate modeling

- Scanning-test-set cross validation
- Measure for surrogate modeling
 - WR2: Weighted coefficient of determination:

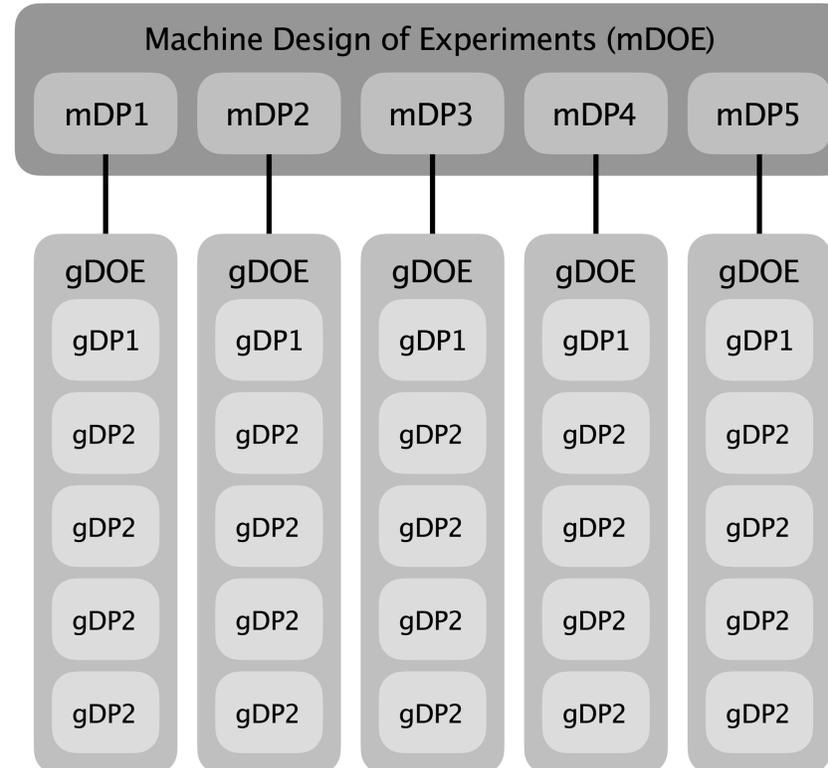
$$WR2 = 1 - \frac{SSE_{\text{Test}} + \alpha SSE_{\text{Training}}}{SST_{\text{Test}} + \alpha SST_{\text{Training}}}$$

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NESTED DESIGN OF EXPERIMENTS

- Separation of machine design space and geometry design space
- First level: machine design of experiments
- Second level: geometry designs of experiments for each machine design

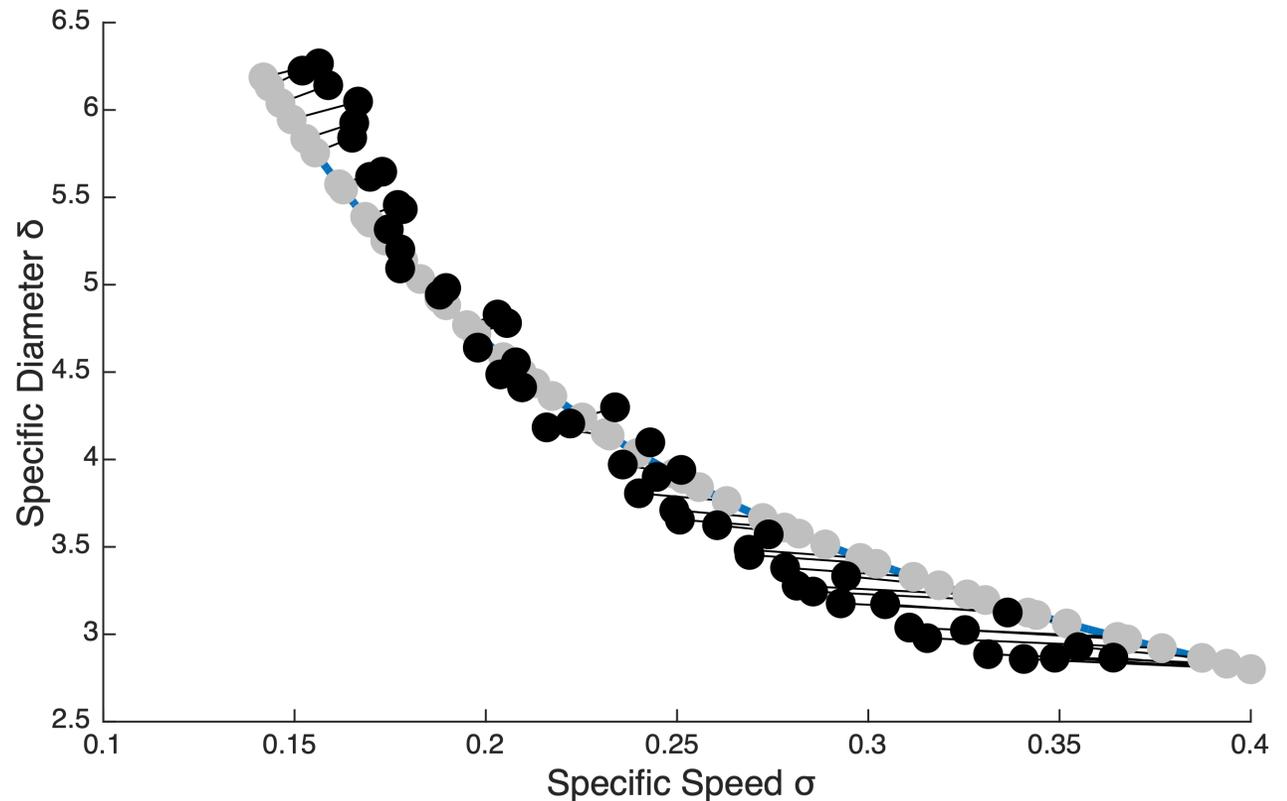


NESTED DESIGN OF EXPERIMENTS

Machine design of experiments

- 50 Machine designs using LHS design

Parameter	Symbol	DOE Properties
<i>Sampled properties</i>		<i>Range</i>
Cordier line position	s_{CORDIER}	0 to 1
Outflow pressure	p_{out}	$2 \times 10^5 \text{ Pa}$ to $4 \times 10^5 \text{ Pa}$
Ambient volume flow rate	\dot{V}_{amb}	$0.5 \text{ m}^3 \text{ s}^{-1}$ to $4 \text{ m}^3 \text{ s}^{-1}$
Axial impeller extent ratio	ν_L	0.2 to 0.4
Trailing edge blade angle	β_2	40° to 75°
Circumferential blade extent	θ_2	35° to 55°
<i>Constant properties</i>		<i>Value</i>
Ambient pressure	p_{amb}	$1 \times 10^5 \text{ Pa}$
Ambient temperature	T_{amb}	288.15 K
Hub to shaft diameter ratio	$D_{1_{\text{hub}}}/D_{\text{shaft}}$	1.25
Blade thickness ratio	ν_s	0.01
Number of blades	z	13



NESTED DESIGN OF EXPERIMENTS

Geometry design of experiments

- 50 geometry designs using LHS design for each machine design point

Parameter	Symbol	DOE Properties
<i>Sampled properties</i>		<i>Range</i>
Hub control points in meridional direction	Hub_Mer	-1 to 1
Hub control points in spanwise direction	Hub_Span	0 to 1
Shroud control points in meridional direction	Shroud_Mer	-1 to 1
Shroud control points in spanwise direction	Shroud_Span	0 to 1
Leading edge hub position	LE_Hub_Pos	0.05 to 0.15
Leading edge offset angle hub to shroud	LE_Shroud_Offset	0° to 10°
Blade twist (Leading Edge)	Twist	-10° to 10°
Blade rake (Trailing Edge)	Rake	-25° to 25°
Intensity of blade's <i>S</i> -shape (<i>hub</i>)	Theta_Hub_S	0 to 1
Intensity of blade's <i>S</i> -shape (<i>shroud</i>)	Theta_Shroud_S	0 to 1

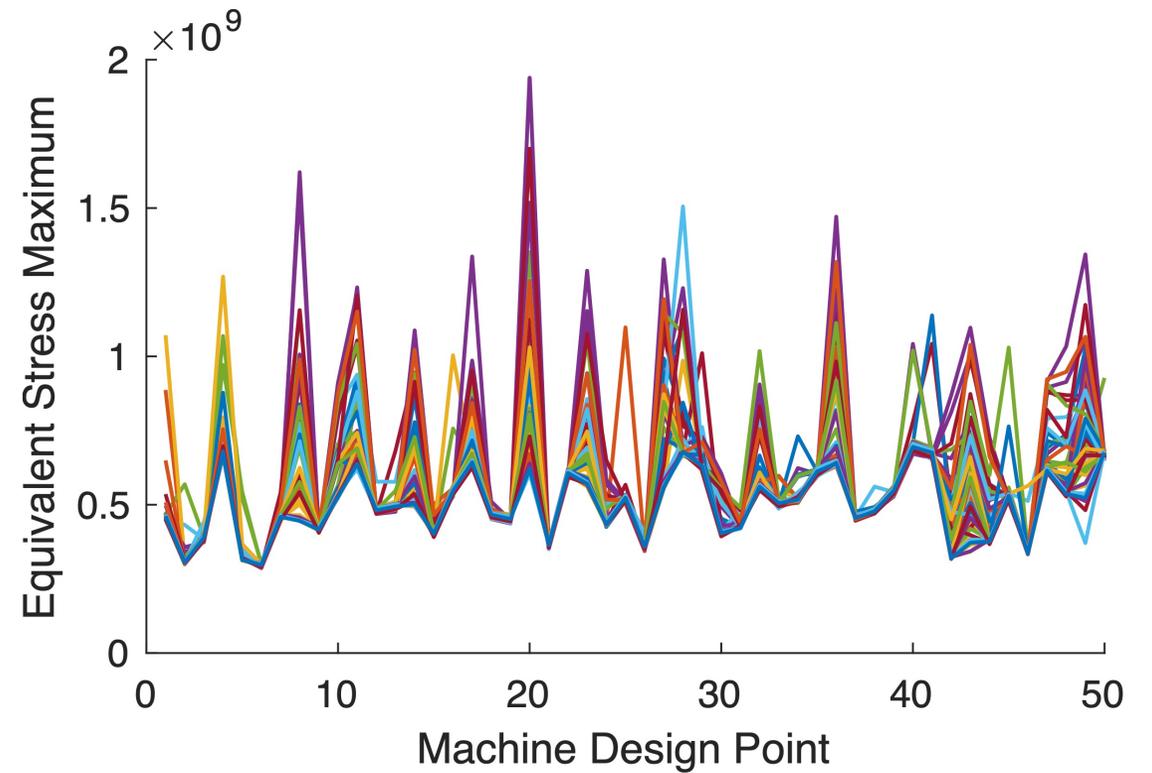
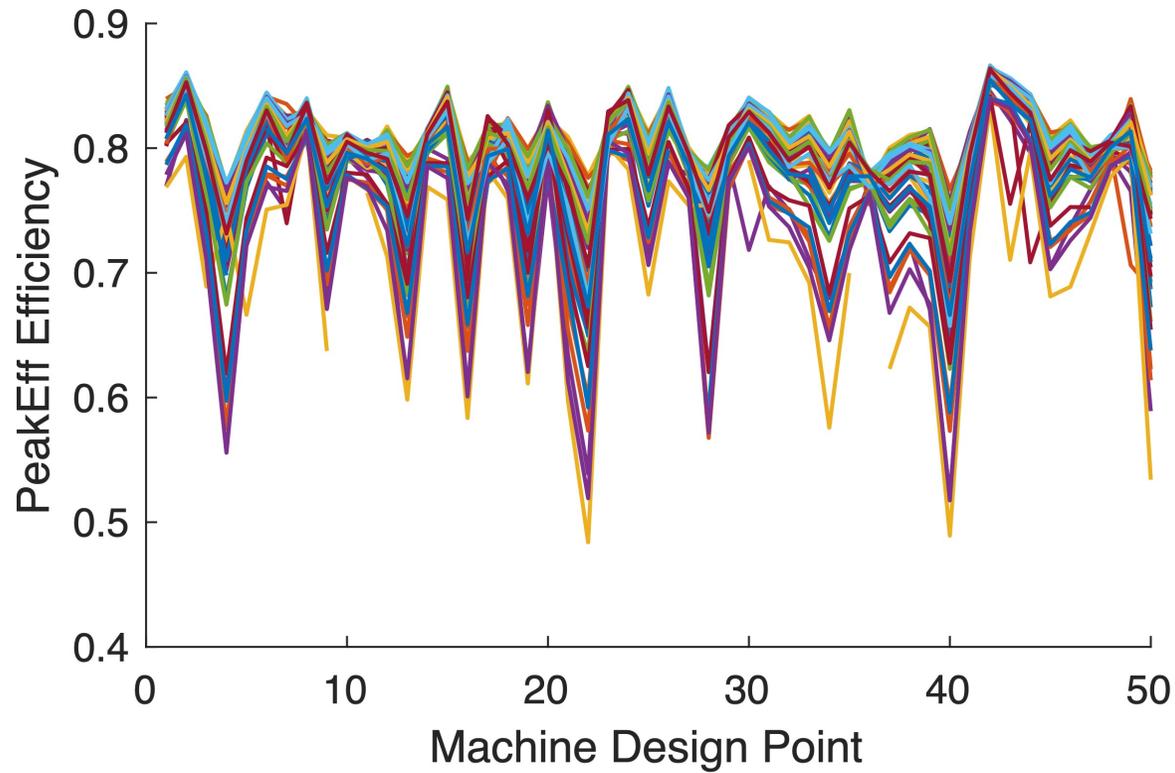
NESTED DESIGN OF EXPERIMENTS

Solving

- CFD
 - 2481 / 2500 successfully computed speed lines
 - More than 19 TB of data
 - More than 35.000 CFD simulations
 - Computational time around 6 months
- FEA
 - All 2500 designs were successfully computed
 - 2.7 TB data

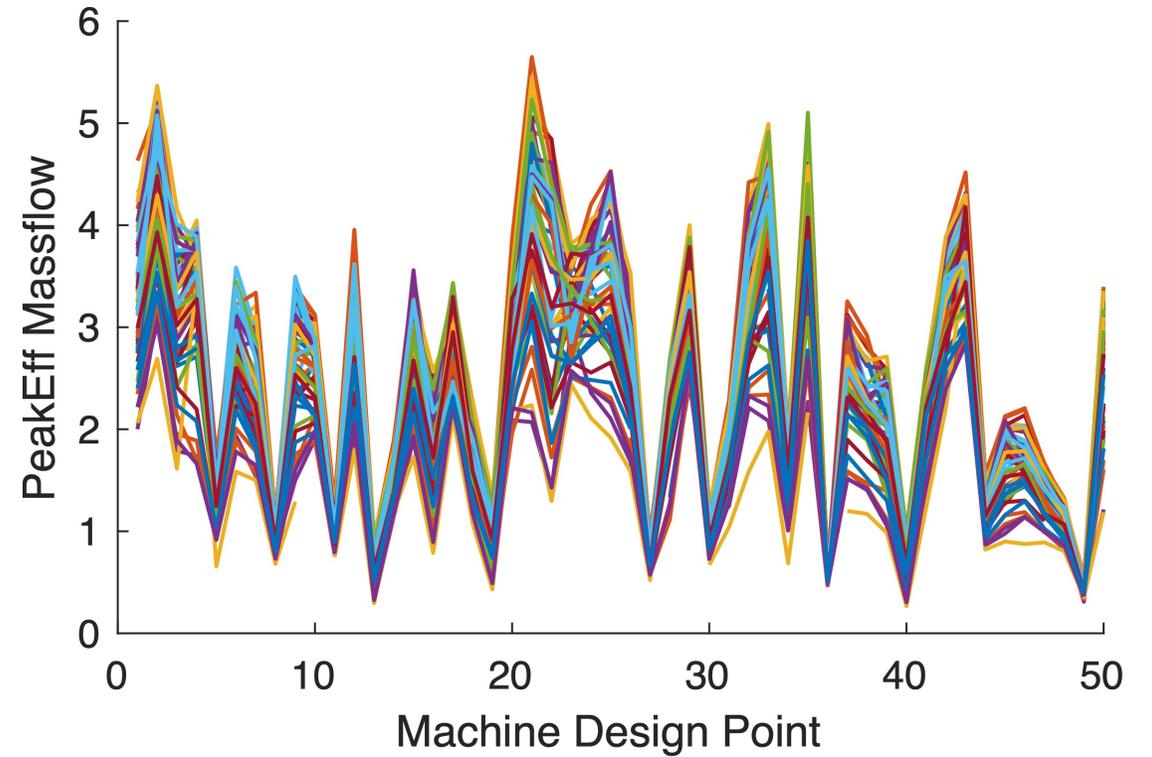
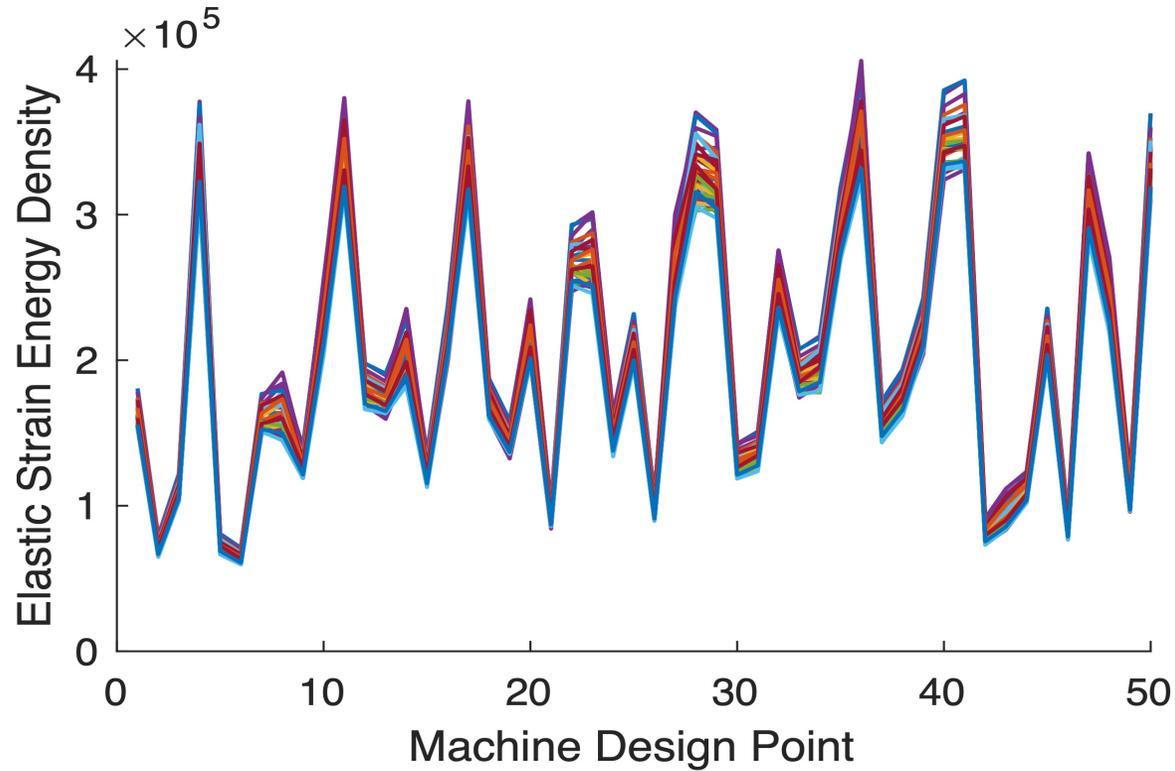
NESTED DESIGN OF EXPERIMENTS

Initial result evaluation



NESTED DESIGN OF EXPERIMENTS

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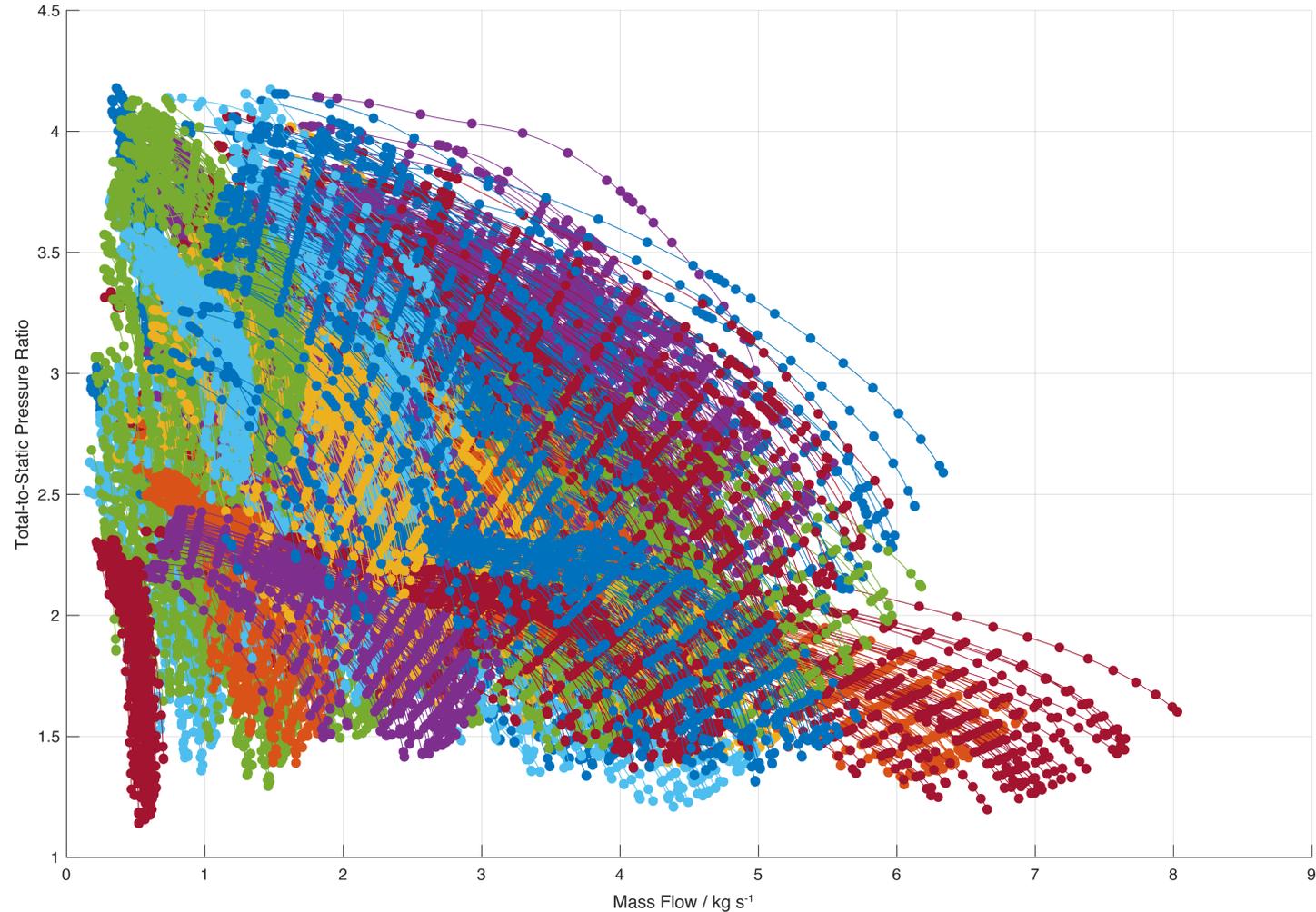


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SURROGATE MODELING

Speed line interpolation

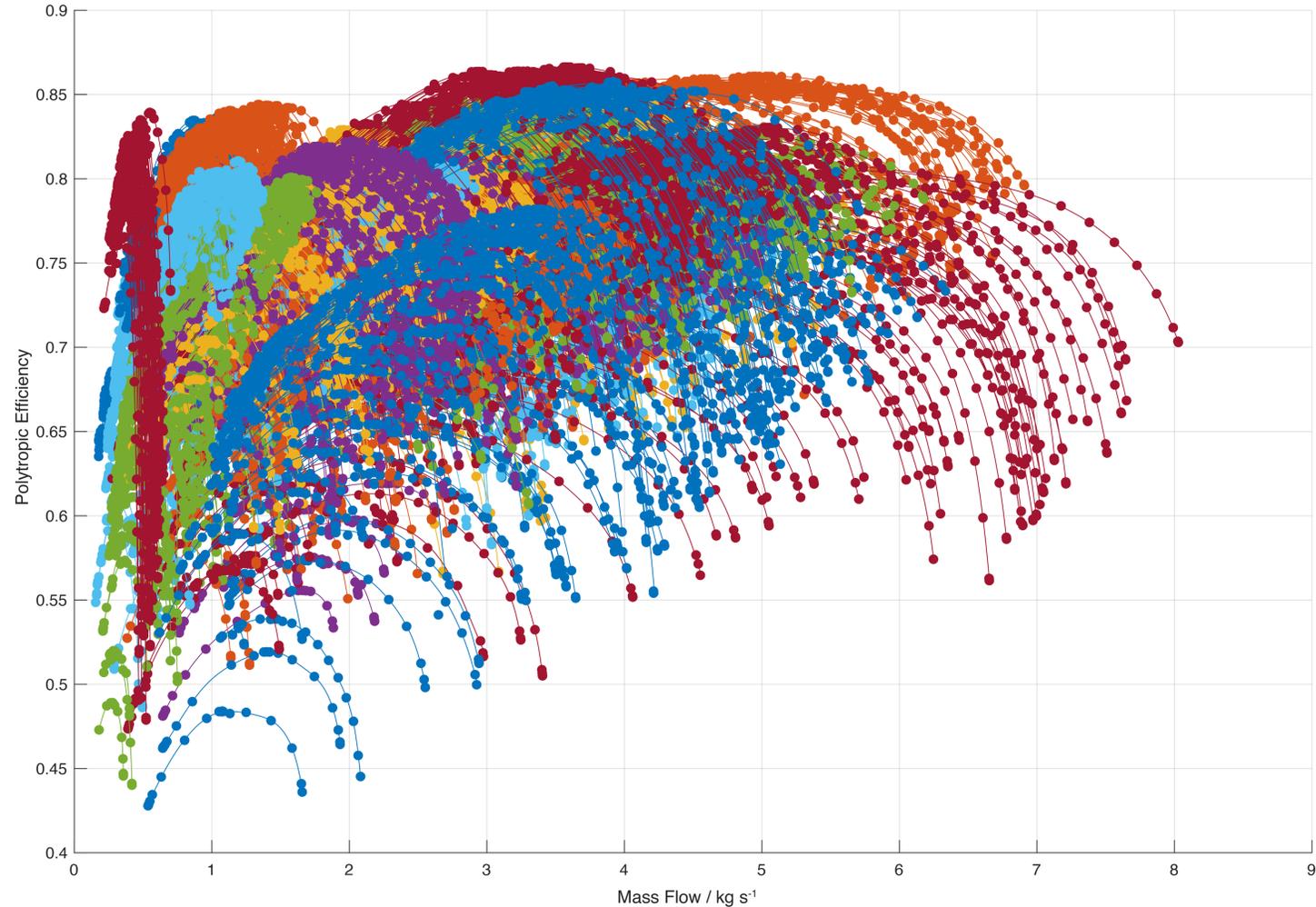
- Modeled as function of exit-corrected mass flow rate:
 - **Mass flow rate**
 - **Total-to-static pressure ratio**
 - Polytropic efficiency
- Additionally, spline fitting was conducted



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Speed line interpolation

- Modeled as function of exit-corrected mass flow rate:
 - **Mass flow rate**
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 - **Polytropic efficiency**
- Additionally, spline fitting was conducted



SURROGATE MODELING

Geometry design of experiments

- Inputs: Geometry design parameters
- Outputs:

Parameter	Symbol	Unit
<i>Speed line parameters</i>		
Peak efficiency	$\eta_{\text{pol}_{\text{max}}}$	—
Peak efficiency mass flow rate	$\dot{m}_{\eta-\text{max}}$	kg s^{-1}
Peak efficiency total-to-static pressure ratio	$\Pi_{\text{t-s}_{\eta-\text{max}}}$	—
Choke efficiency	$\eta_{\text{pol}_{\text{choke}}}$	—
Choke mass flow rate	\dot{m}_{choke}	kg s^{-1}
Choke total-to-static pressure ratio	$\Pi_{\text{t-s}_{\text{choke}}}$	—
Surge efficiency	$\eta_{\text{pol}_{\text{surge}}}$	—
Surge mass flow rate	\dot{m}_{surge}	kg s^{-1}
Surge total-to-static pressure ratio	$\Pi_{\text{t-s}_{\text{surge}}}$	—
Normalized speed line width	$\Delta \dot{m}_{\text{norm}}$	—
Total-to-static pressure ratio spline parameter (\dot{m} -coordinate)	$\chi_{\text{TSPR}_{\dot{m}}}$	—
Total-to-static pressure ratio spline parameter ($\Pi_{\text{t-s}}$ -coordinate)	$\chi_{\text{TSPR}_{\Pi_{\text{t-s}}}}$	—
Polytropic efficiency spline parameter (\dot{m} -coordinate)	$\chi_{\text{Eff}_{\dot{m}}}$	—
Polytropic efficiency spline parameter (η_{pol} -coordinate)	$\chi_{\text{Eff}_{\eta}}$	—

<i>Structural load parameters</i>		
Maximum value of the von Mises stress	$\sigma_{v_{\text{max}}}$	Pa
Maximum value of the deformation	$\Delta \mathbf{X}_{\text{max}}$	m
Directional deformation of the leading edge at the shroud, collinear	Δb_{LE}	m
Directional deformation of the trailing edge at the shroud, collinear	Δb_{TE}	m
Elastic strain energy of the full impeller model	U_{impeller}	J
Elastic strain energy of the blade region	U_{blade}	J
Elastic strain energy of the disc region	U_{disc}	J
Elastic strain density of the full impeller model	u_{impeller}	J m^{-3}
Elastic strain density of the blade region	u_{blade}	J m^{-3}
Elastic strain density of the disc region	u_{disc}	J m^{-3}
Volume of the full impeller model	V_{impeller}	m^3
Volume of the blade region	V_{blade}	m^3
Volume of the disc region	V_{disc}	m^3

SURROGATE MODELING

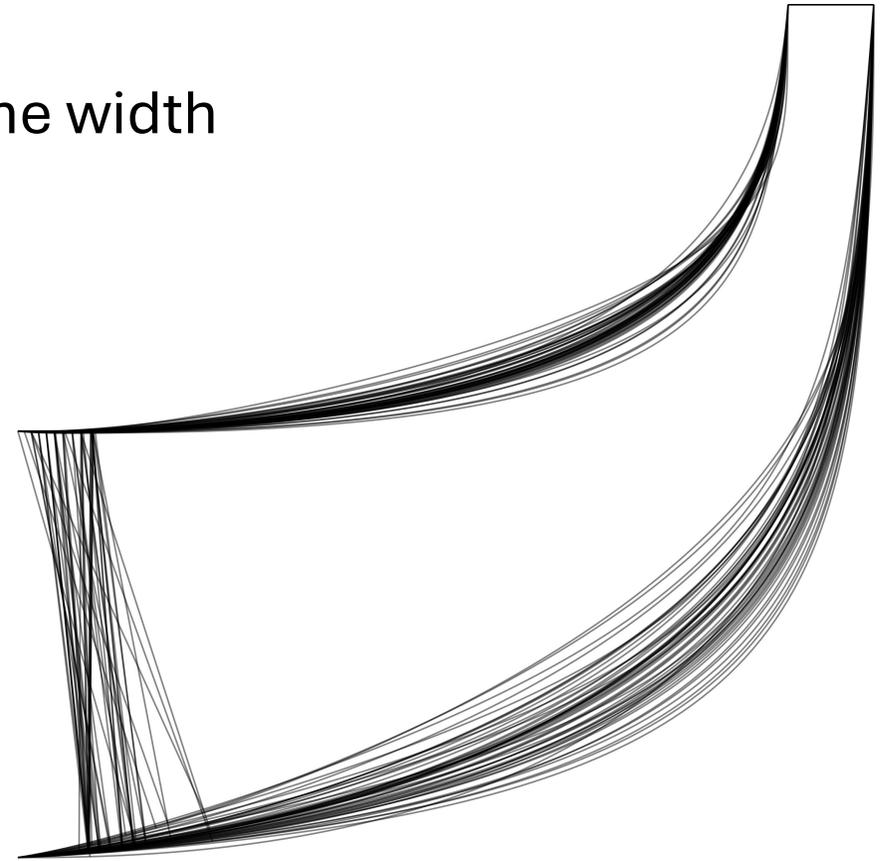
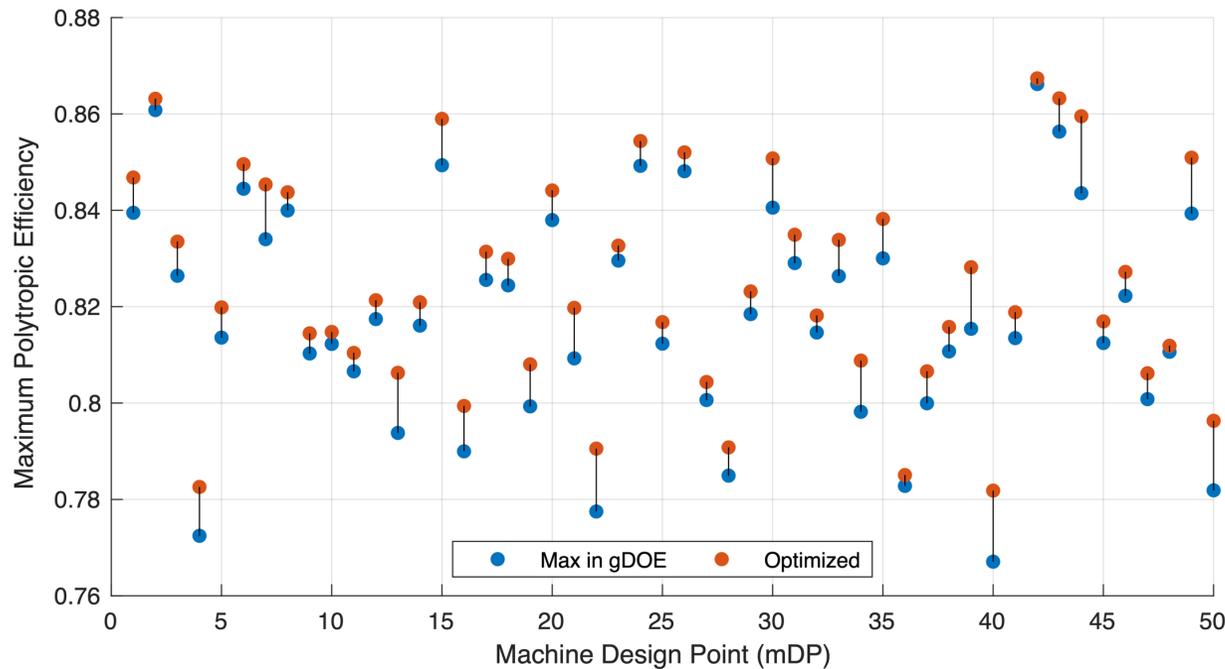
Geometry design of experiments

- Hybrid surrogate model is trained 50 times (each machine design point) for each output parameter = 1350 surrogate models
- Mean WR2 = 0.9483

SURROGATE MODELING

Machine design point-wide optimization

- Optimization of geometry design parameters for each machine design point:
 - Achievable efficiency and achievable speed line width



SURROGATE MODELING

Machine design of experiments

Inputs:

Sampled:

- Ambient volume flow rate
- Total-to-static pressure ratio
- Axial impeller extent ratio
- Circumferential blade extent
- Impeller exit relative blade angle

Derived:

- Specific diameter
- Specific speed
- Flow coefficient
- Polytropic work coefficient
- Chord Reynolds number

• Outputs:

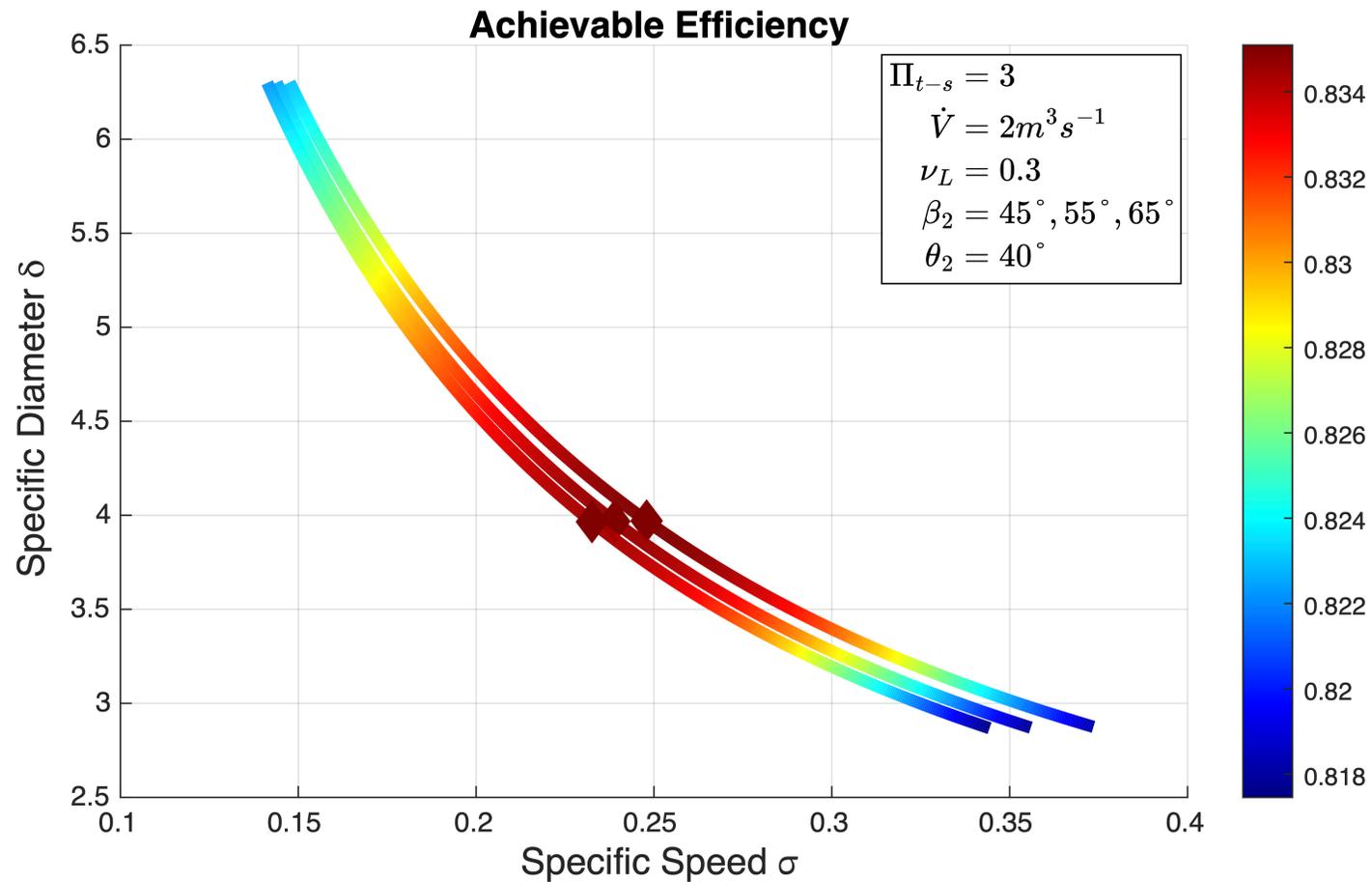
- Achievable Efficiency
 - Achievable Speed Line Width
 - Associated speed line parameters
 - Associated geometry parameters
 - Machine design point-wide structural result parameters
- WR2 for main parameters > 0.99

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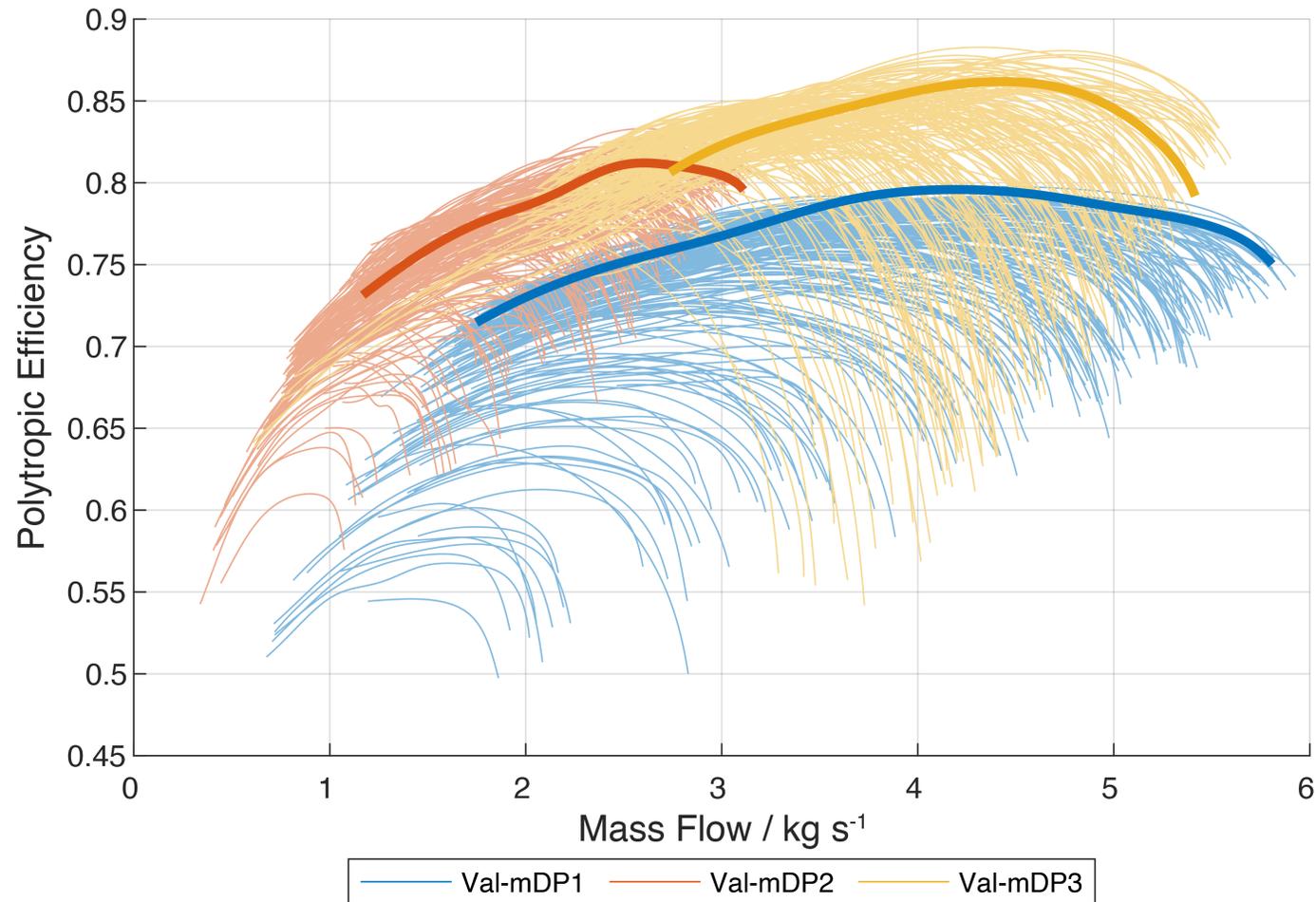
RESULTS

Duty-specific Cordier lines



RESULTS

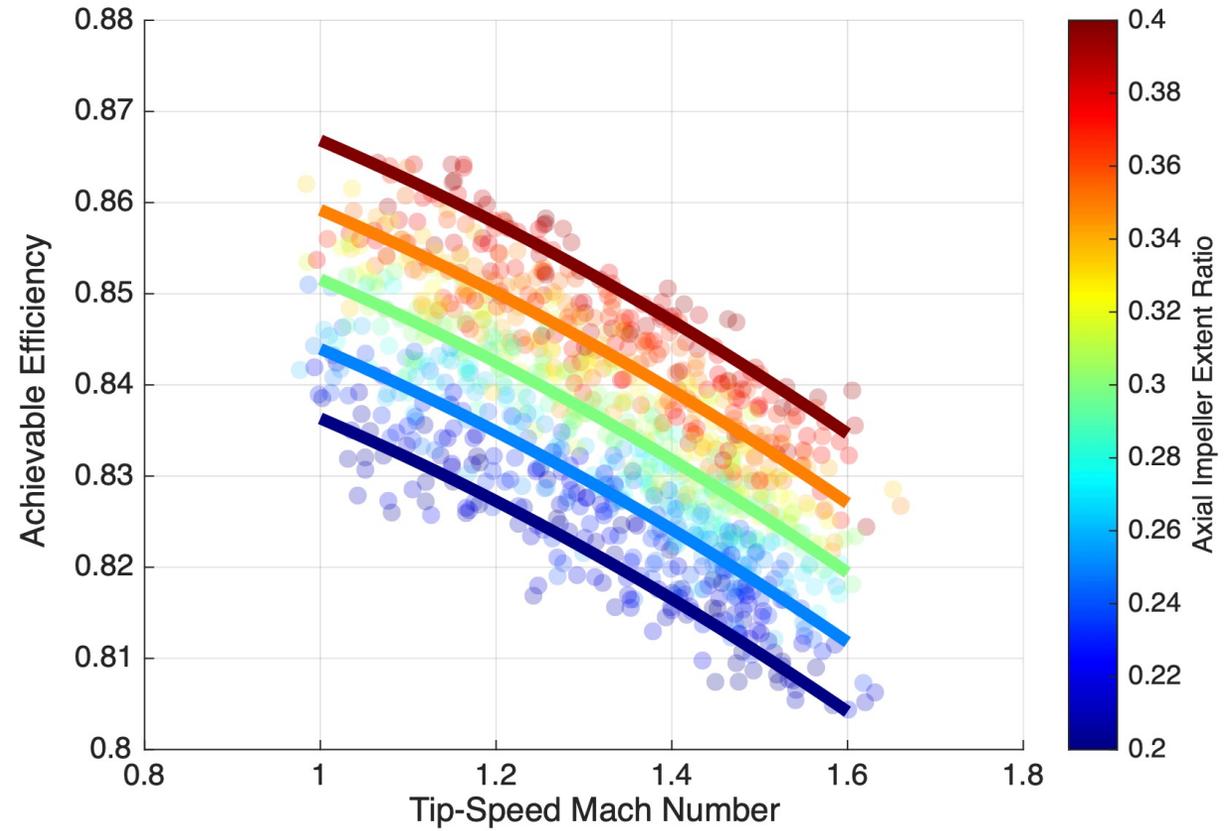
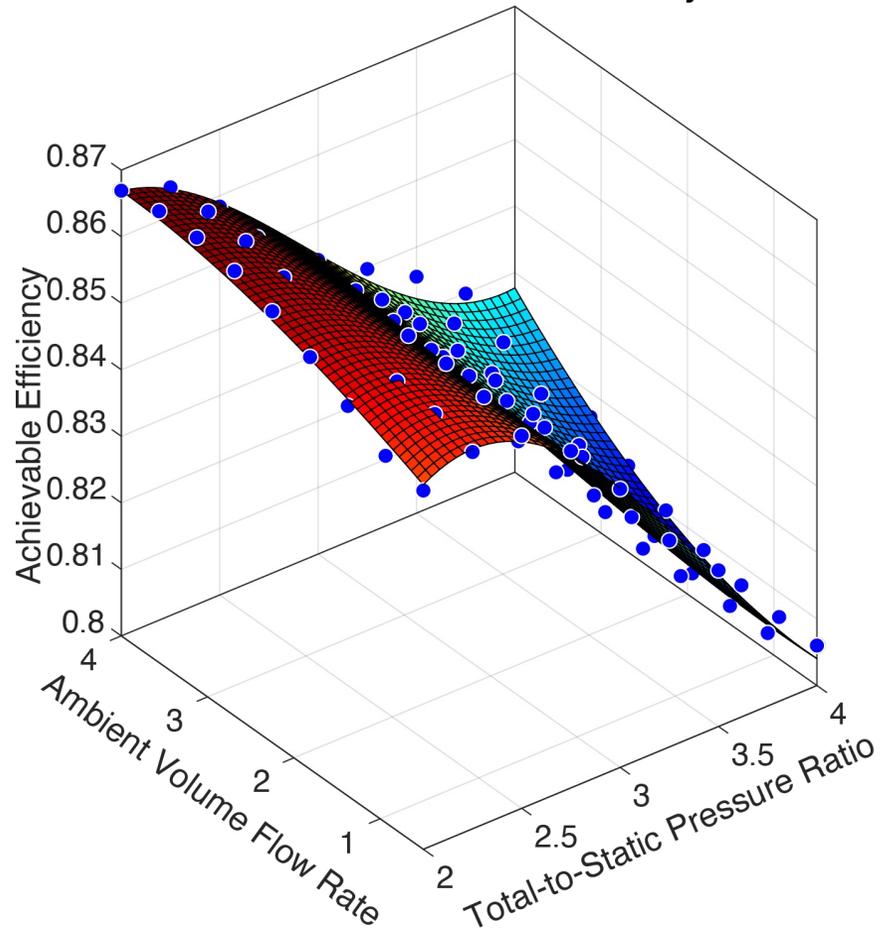
Direct optimization, initial guess for impeller geometry

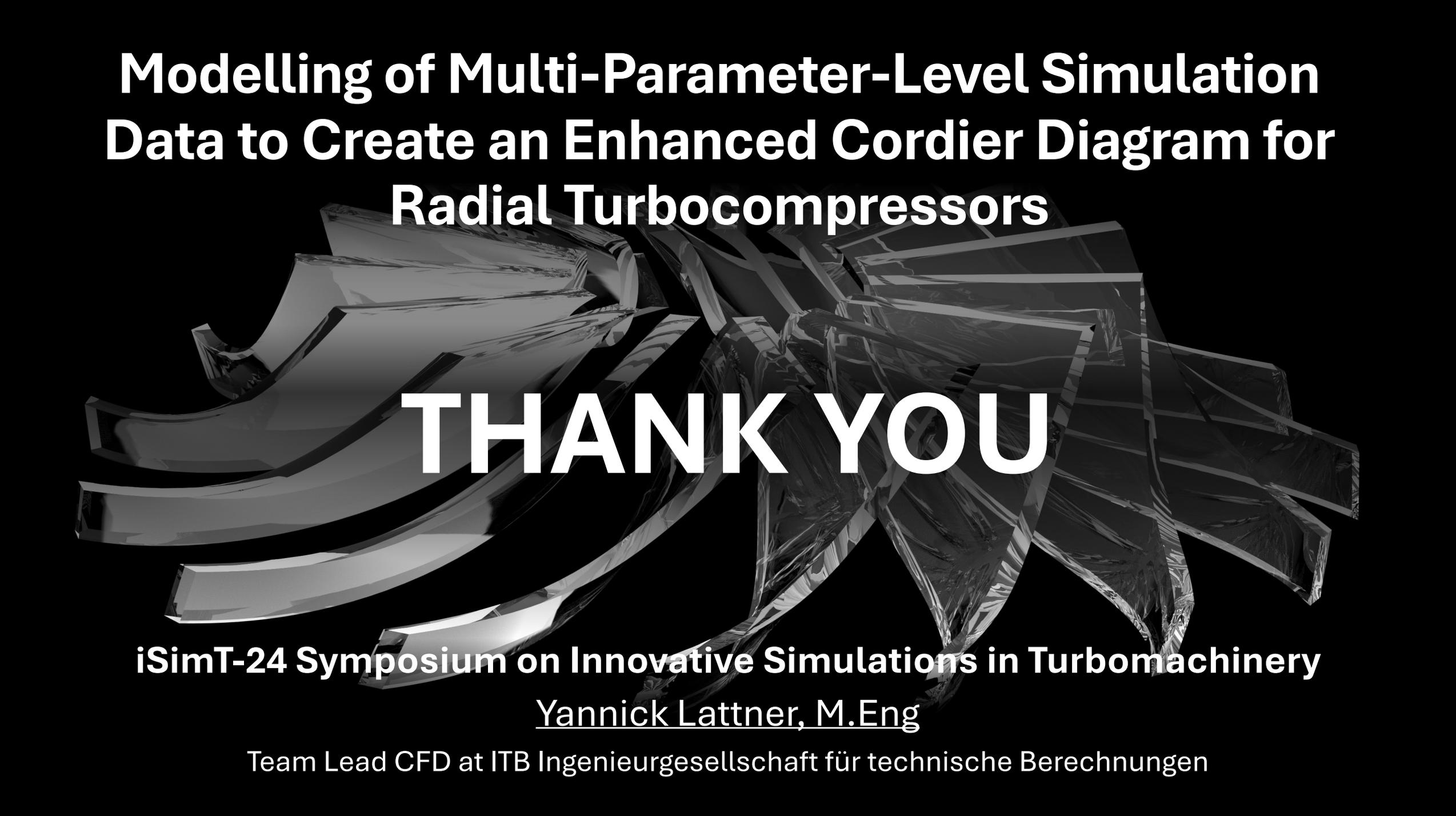


RESULTS

Efficiency correlations

Fit: Achievable Efficiency





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THANK YOU

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